

ECE 421: Electronics for Instrumentation

MEMS Technology **MEMS Inertial Sensors**

Dr. Mohamed El-Sheikh & Dr. Mostafa Soliman

Email: melsheikh.mahmoud@icl.asu.edu.eg

Outline

□ MEMS-Based Gyroscopes

- Structure and concept

- Specifications

- Categories

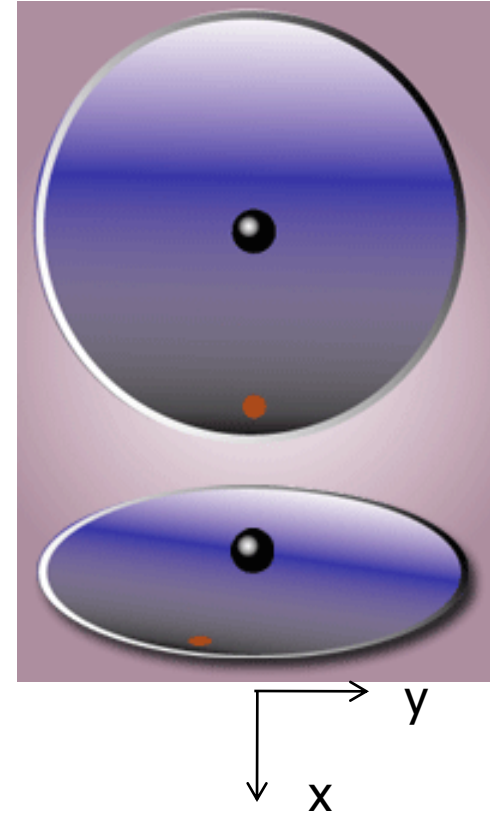
Gyroscopes

- Structure and concept
- Architectures
- Specifications

Vibratory Gyroscope Operation Principle

- Vibratory Gyroscopes are based on the **Coriolis force effect**.
- The **Coriolis force** affects objects moving in a rotating frame.
- Only seen in the rotating frame and so called **fictional force**.
- All vibratory gyroscopes are based on the **Coriolis Effect**: In a reference frame rotating at angular velocity Ω , a mass M moving with velocity V sees a force:

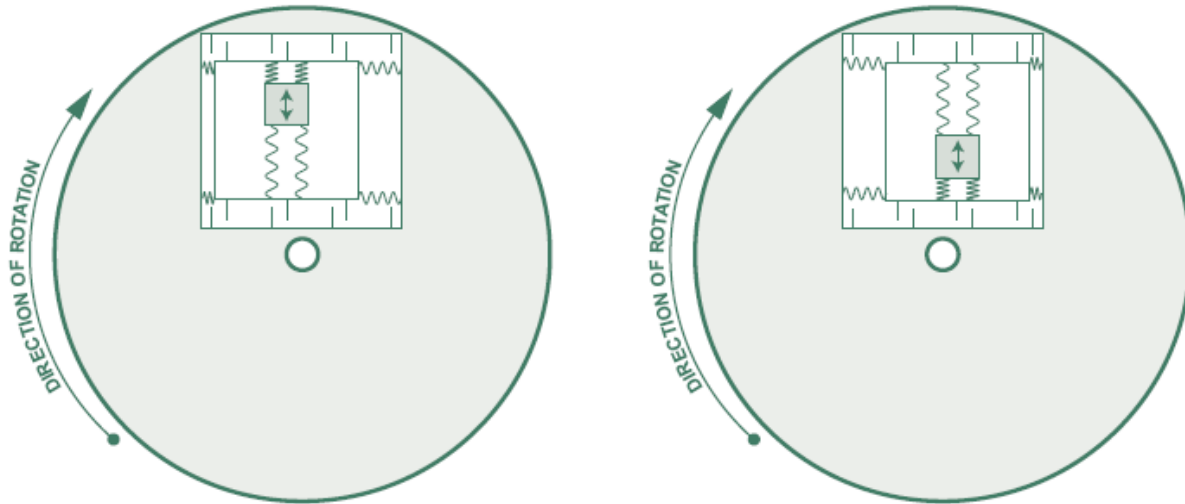
$$F = 2M (V \times \Omega)$$



Coriolis force (F_y) = $-2m\Omega_z v_x$

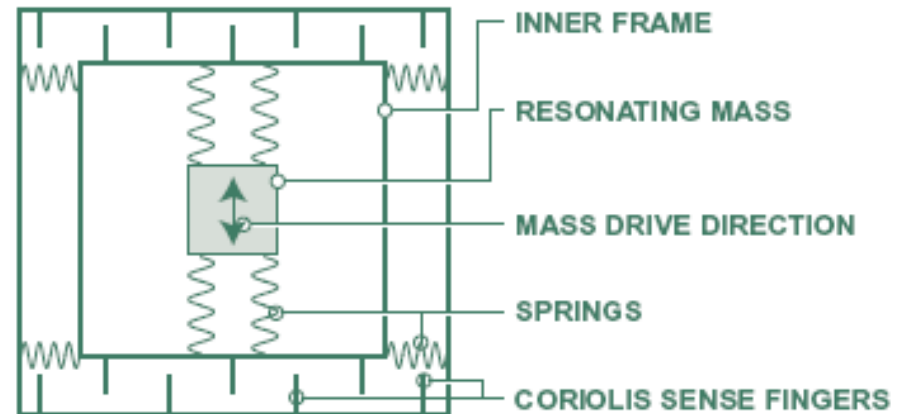
Coriolis Effect in Sensors

- On the rotating surface, a sensor element is **vibrating** in say the **Y** direction, a coriolis force will result in the perpendicular **x** direction.
- If the element is also free to move in x direction, a measure of its displacement could be used to measure the rotation rate in the **z** direction



Coriolis Sensor Device

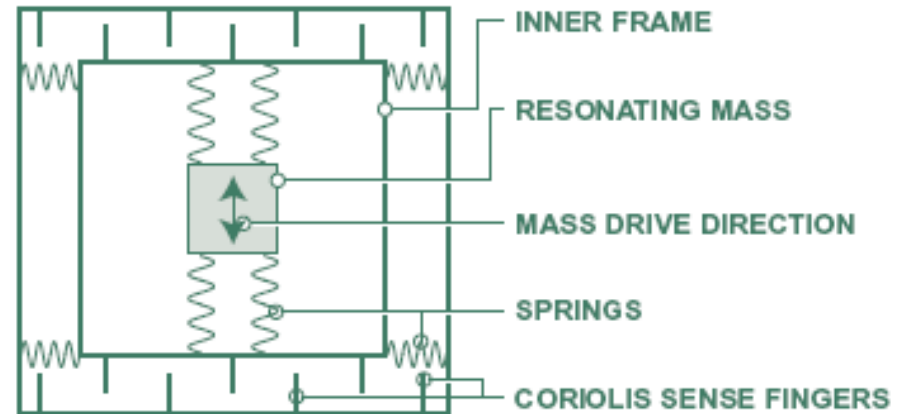
- The Coriolis Sensor device is a Mass that should
 - Have two degrees of mechanical freedom
 - Be Actuated to vibrate/move in one dimension
 - Be position sensed in another perpendicular direction



MEMS Gyro = Actuator + Sensor (Accelerometer)

Coriolis Vibratory Gyroscopes Concept

- Based on energy transfer between two orthogonal vibrations modes: **the drive-mode and sense-mode** (uncoupled at rest)



- With rotations, **Coriolis force** couples the modes and the drive-mode excites the sense-mode
- The sense-mode vibration amplitude is **a measure** of the of the rotation rate
- The fundamental challenge is that **Coriolis force is very small** and has to be measured in the presence of much larger electrical signals

Example: Coriolis force on a vibrating mass

□ Let $x=1 \mu\text{m} \sin(2\pi 10^4 t)$, $m=0.6 \text{ nkg}$, $\Omega_z=2\pi \text{ rad/s}$

□ Then, the velocity is given by the $v_x=dx/dt$:

$$v_x = 2\pi * 10^4 * 1 \mu \cos(2\pi 10^4 t)$$

□ The Coriolis force is given by $F_y = -2m\Omega_z v_x$

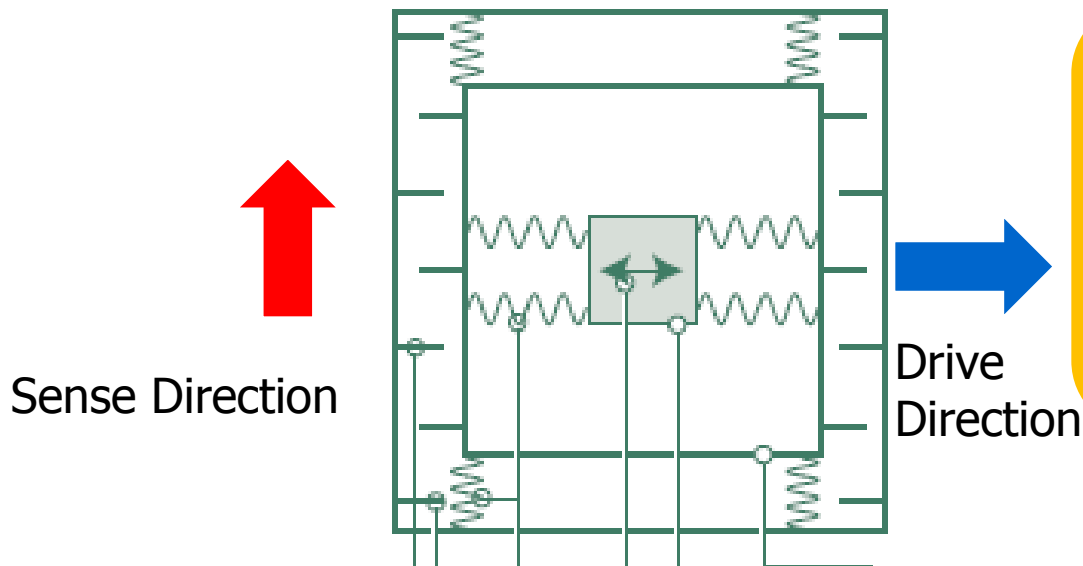
□ Therefore, Coriolis force due to ($\Omega_z = 2\pi$)

$$\begin{aligned} F_y &= -2 * 0.6 \text{ n} * 2\pi * 2\pi * 10^4 * 1 \mu \cos(2\pi 10^4 t) \\ &= -0.24 \text{ nN} \cos(2\pi 10^4 t) \end{aligned}$$

□ Very small oscillation at the resonance frequency but -90° out-of-phase with the x-displacement

What is the main blocks in a vibratory gyroscope ?

- A suspended mass moving in the **drive direction** (drive mode) using an actuator.
- A suspended frame that is allowed to move in the **sense direction** due to Coriolos force.



□ This is a 2 DOF system.

□ $F_c = 2 m v_d \cdot \Omega_z$

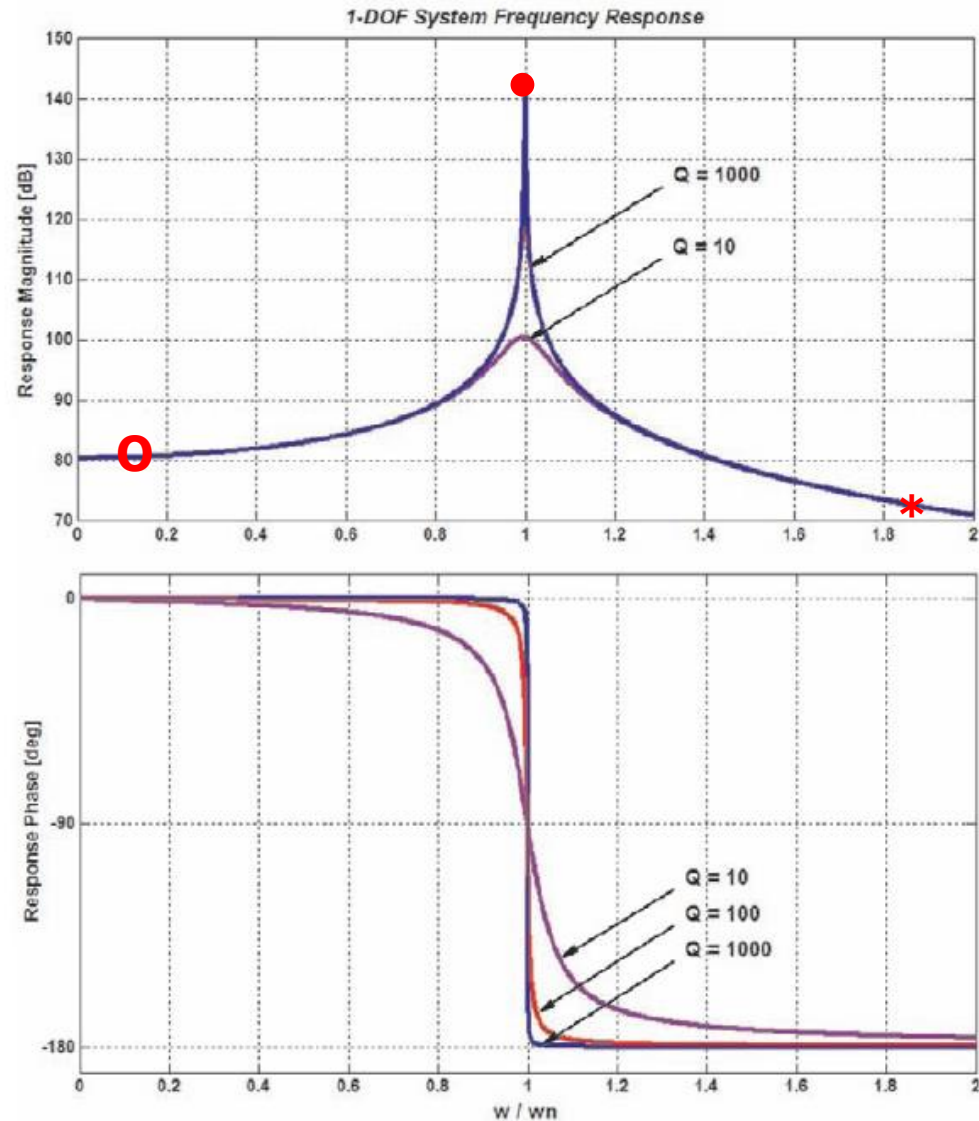
Drive Operation

□ We should work in point
“ \bullet ” for maximum drive
displacement .

□ $x_d = x_{od} \sin(\omega_{nd} t)$

□ $v_d = \omega_{nd} x_{od} \cos(\omega_{nd} t)$

□ $F_c = 2M \cdot v_d \cdot \Omega$



Coriolos Force Cases

□ If Ω is constant: ($\Omega = \Omega_o$)

$$F_c = 2M \cdot \omega_{nd} x_{od} \Omega_o \cos(\omega_{nd}t)$$

■ F_c has the same frequency of drive displacement but with a 90 degree phase shift.

□ If Ω is harmonic: ($\Omega = \Omega_o \cos(\delta t)$)

$$F_c = 2M \cdot \omega_{nd} x_{od} \Omega_o \cos(\omega_{nd}t) \cos(\delta t)$$

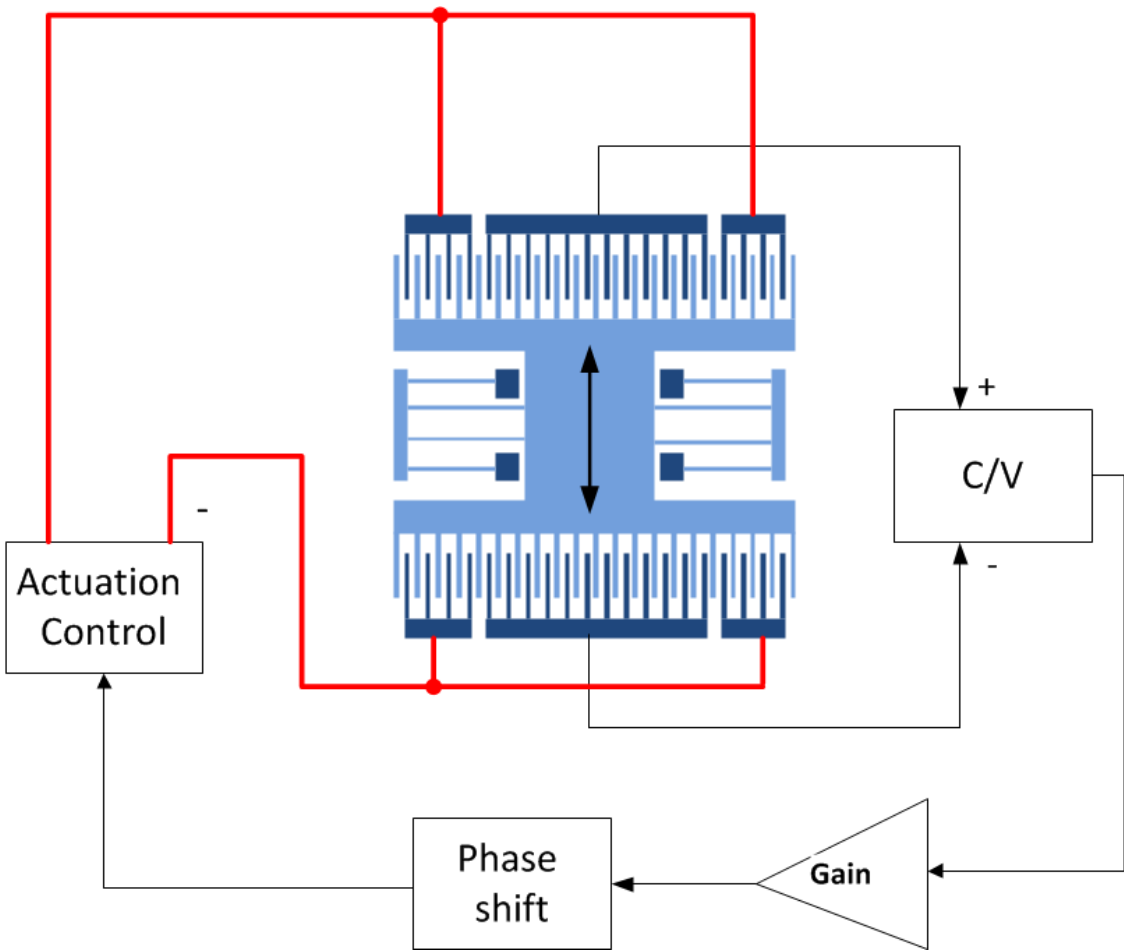
$$= M \cdot \omega_{nd} x_{od} \Omega_o [\cos(\omega_{nd} - \delta)t + \cos(\omega_{nd} + \delta)t]$$

■ F_c is an DSSC signal (Double side band suppressed carrier)

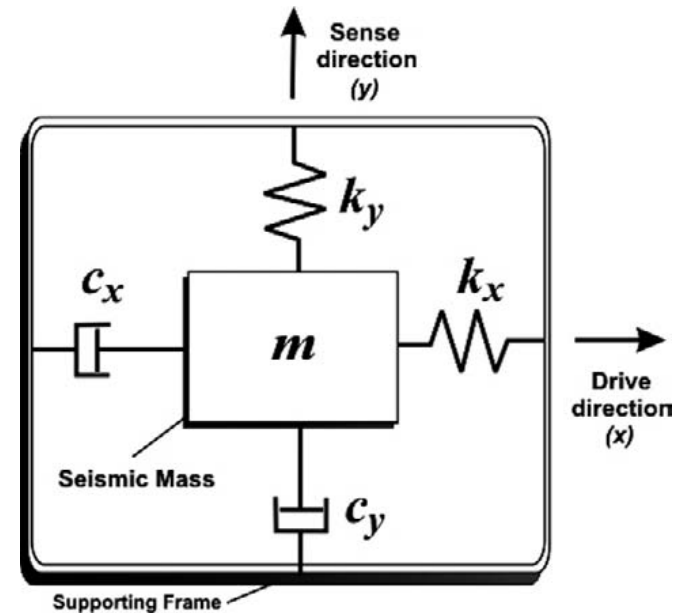
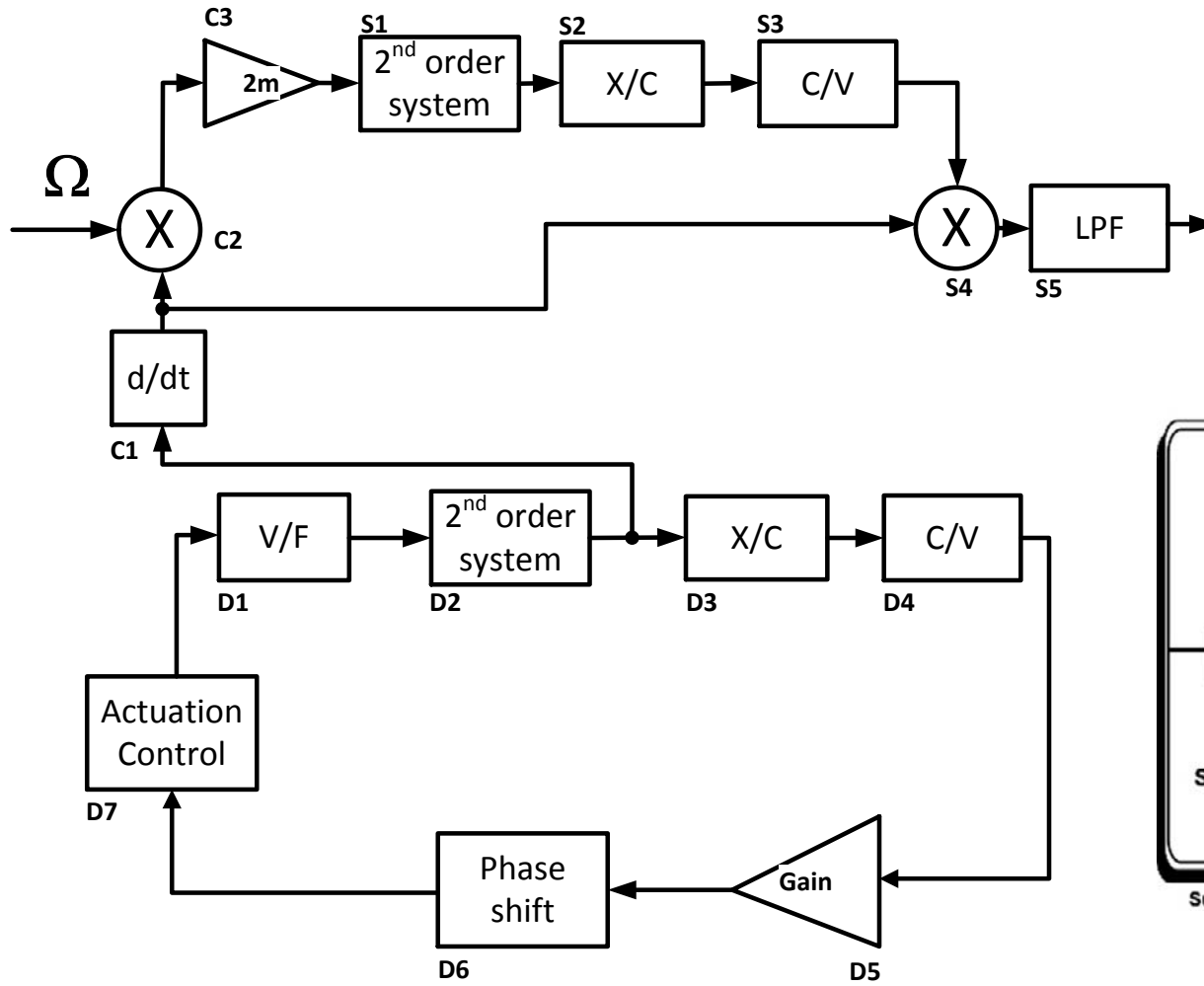
Drive frequency variation

- During fabrication, ω_{nd} will vary from one part to another.
- Therefore, actuating the drive mode at constant frequency may lead to miss the peak of the frequency response.
- Therefore, we need to find a method to operate on the frequency of the peak response whatever its value is
 - ⇒ It makes the drive mode operate as a resonator instead of actuator

How to make a resonator ?



System Overall Block Diagram



MEMS Gyroscope (Part II)

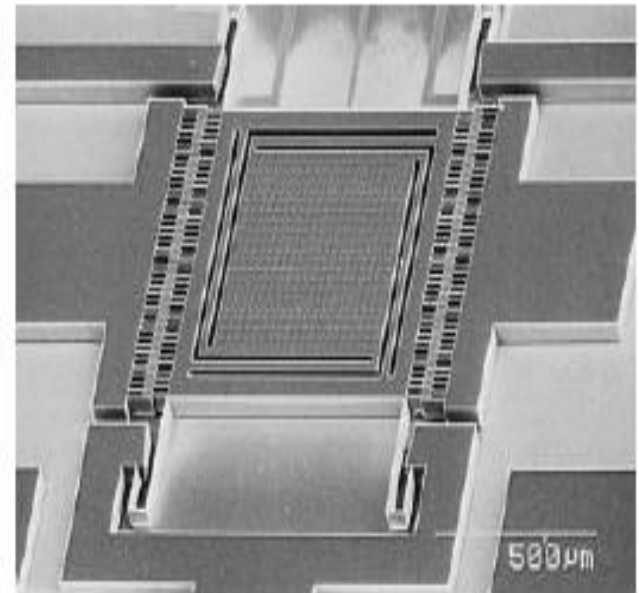
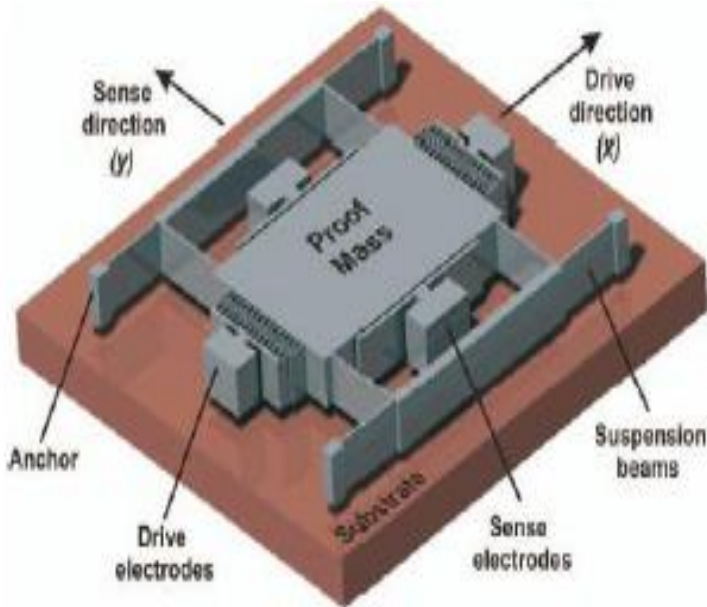
- Structure and concept
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MEMS Gyro Design Varies Significantly

- Since its introduction, the comb-drive actuation and parallel-plate sensing has been the prevalent design
- Drive-mode and sense-mode resonance frequency varies between matching to completely separated.
- Some gyroscopes uses just one proof mass for both drive- and sense-mode but others use two or more masses to further to further decouple the drive- and sense-modes

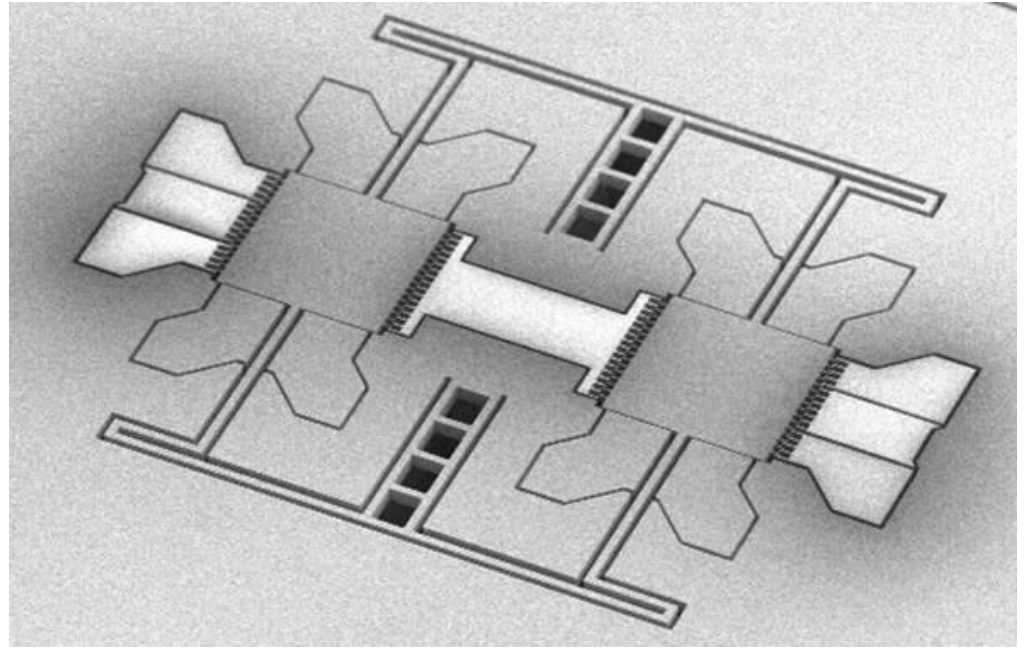
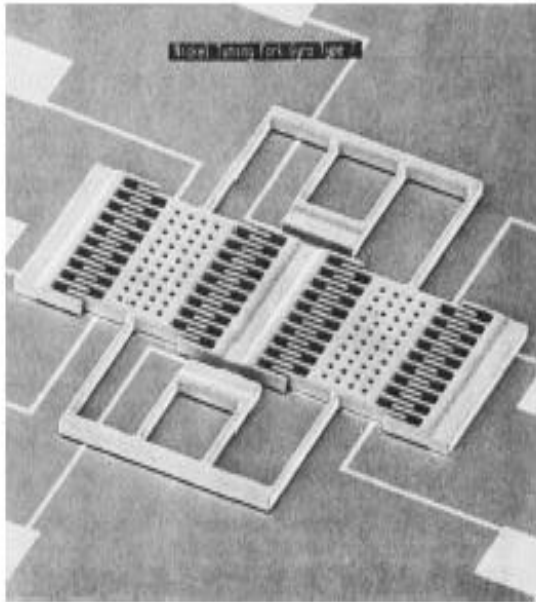
Proof Mass Gyroscopes

- Most reported MEMS gyroscopes
- Linear acceleration can be filtered out by using accelerometers (IMU)
- Can be in-plane or out-of-plane



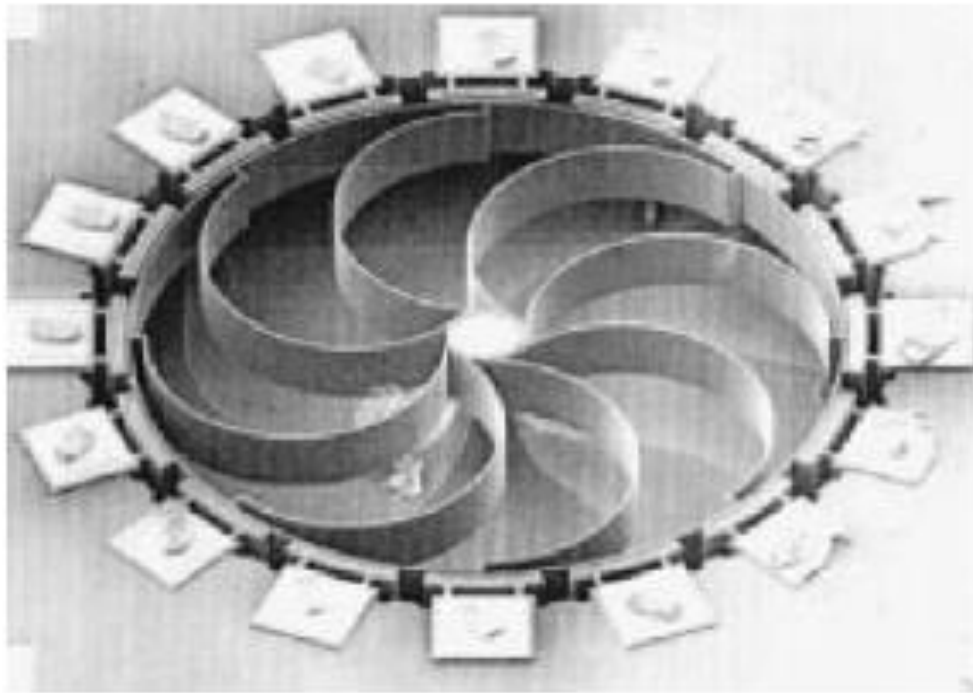
Tuning Fork Gyroscopes

- Dependence of the output signal on linear acceleration can be electronically rejected.
- Reduces energy losses as no net motion at the junction and therefore can be mounted inertial stable at this junction.



Vibrating Rings

- Highest performance (reduced spurious vibrations, increased sensitivity and decreased temperature dependence)



MEMS Gyroscope (Part II)

- Structure and concept
- Specifications

Gyroscope Specifications

- Full- scale range [$^{\circ}/s$]
- Resolution [$^{\circ}/(s/\sqrt{\text{Hz}})$]
- Scale factor: [$V/(^{\circ}/s)$].
- Zero rate output
- Angular random walk
- Bias drift: The peak-to-peak value of the **slowly** varying output in the absence of a rotation rate [$^{\circ}/s$ or $^{\circ}/h$]
- Maximum allowable shock (g in ms)

Gyroscope Grades

Parameters	Rate grade	Tactical grade	Inertial grade
Angle random walk ($^{\circ}/\sqrt{h}$)	>0.5	0.5 – 0.05	<0.001
Bias drift ($^{\circ}/h$)	10 – 1000	0.1 – 10	<0.01
Scale factor accuracy (%)	0.1 – 1	0.01 – 0.1	<0.001
Full scale range ($^{\circ}/s$)	50 – 1000	>500	>400
Max. shock in 1s, g's	10^3	$10^3 – 10^4$	10^3
Bandwidth (hz)	>70	~ 100	~ 100

Mechanical Gyroscopes
Ring Laser Gyroscopes
Fiber-optics Gyroscopes
MEMS/MOEMS